Electromagnetic ice absorption rate at Dome C, Antarctica

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ABSTRACT. Radio-echo sounding (RES) is a radar technique widely employed in Antarctica and Greenland to define bedrock topography but, over the last decade, it has also played an important role in subglacial lake exploration and hydrogeological studies at the bedrock/ice interface. In recent studies, bedrock characterization has been improved through analysis of radar power echoes to evaluate the electromagnetic (EM) properties of the interface and allow the distinction between wet and dry interfaces. The RES received signal power depends on ice absorption and bedrock reflectivity, which is closely linked to the specific physical condition of the bedrock. In this paper, an evaluation of EM ice absorption was conducted starting from RES measurements collected over subglacial lakes in Antarctica. The idea was to calculate ice absorption starting from the radar equation in the case of subglacial lakes, where the EM reflectivity value is considered a known constant. These values were compared with those obtained from analysis of ice-core dielectric profiles from EPICA ice-core drilling data. Our analysis reveals that the ice absorption rate calculated from RES measurements has an average value of 7.2 dB km⁻¹, and it appears constant, independent of the subglacial lake depth in different zones of the Dome C area.

KEYWORDS: Antarctic glaciology, ice physics, radio-echo sounding, subglacial lakes

INTRODUCTION

Radio-echo sounding (RES) is an active remote-sensing technique that utilizes electromagnetic (EM) waves that penetrate into ice. This technique is used to obtain information about the EM properties of different interfaces that reflect an incident signal back to the acquisition system (Plewes and Hubbard, 2001). RES surveys have been widely employed in Antarctic ice sheet exploration and are considered an indispensable tool for mapping bedrock morphologies and properties. Moreover, the discovery of numerous subglacial lake areas (entrapped in the ice sheet) has attracted scientific interest in the possible existence of water circulation between lakes or beneath the ice (Kapitsa and others, 1996; Rémy and others, 2003; Tabacco and others, 2006; Wingham and others 2006; Bell and others 2007; Carter and others 2009). While differences in echo strength between rock and lake surfaces can often be clearly differentiated in radargrams (high signal level in a flat shape), this is not true of wet and dry rock surfaces. An increase in signal amplitude from bedrock can be ascribed to several different factors (e.g. a focusing effect, surface roughness, or changes in the EM properties of the ice column). Furthermore, the presence of unconsolidated sediments (water-saturated or not) must be considered as at least probable, which further complicates understanding of the ice/bedrock interface properties.

Observation of the power of radar echoes can help resolve this problem, extending the significance of a RES dataset and enhancing its final interpretation (Oswald and Gogineni, 2008; Paden and others, 2010). In recent years this kind of study has became a powerful tool to investigate and highlight the physical properties of bedrock, with important results that include establishing the presence of different kinds of subglacial lakes, the existence of extensive wet areas, and the possibility of observing hydrological exchange connections under the Antarctic ice sheet (Carter and others, 2007; Zirizzotti and others, 2012). The power of the echoes can be assessed by solving the radar equation that takes into account each term (Bogorodsky and others, 1985), with EM ice absorption, geometrical spreading, medium focusing, and reflectivity being the main contributing factors.

EM ice absorption can be assessed both from ice-core drilling measurements and from RES measurements. Using ice-core drilling data, information can be obtained about ice absorption rate along the ice column. Detailed evaluation can be found in several papers: Carter and others (2009) analyzed bedrock reflectivity in the Dome C (East Antarctic ice sheet) area using a self-consistent model; Eisen and others (2006) evaluated RES radargram amplitude with icecore dielectric profile (DEP)-conductivity measurements from Dronning Maud Land, Antarctica; Fujita and others (2012) studied RES response in East Antarctica; Jacobel and others (2010) studied radar-attenuated signals in East Antarctica along a traverse route; Matsuoka and others (2012) predicted radar attenuation across the Antarctic ice sheet; MacGregor and others (2012) examined the spatial variation of radar attenuation in detail for the Vostok (East Antarctica) flowline; and Zirizzotti and others (2010) evaluated ice absorption rate from RES measurements in wet and dry zones in the Dome C area.

This paper aims to integrate and verify ice column absorption (as an important factor in the radar equation) by comparing data from EPICA (European Project for Ice Coring in Antarctica) Dome C ice cores to data obtained from RES echoes recorded over catalogued subglacial lakes (where the EM reflectivity is known) chosen in the area surrounding the ice-core site. The main aim is to investigate how this particular physical property might vary with distance starting from a known calibrated measurement.

MODELING ICE ABSORPTION

In a homogeneous low-loss EM medium with complex relative dielectric permittivity $\varepsilon_r = \varepsilon' - j\varepsilon'' = \varepsilon' - j\sigma/(\varepsilon_0\omega)$, the absorption loss rate *A* (dB m⁻¹) depends on the complex



Fig. 1. Corrected ice conductivity (red line) and temperature (blue line) at EPICA drilling site.

dielectric permittivity according to

$$A = 8.686 \sqrt{\frac{\mu_0}{\varepsilon_0 \varepsilon'}} \frac{\sigma}{2} \tag{1}$$

where ε_0 and μ_0 are the free-space dielectric permittivity and magnetic permeability respectively, while σ is the electrical conductivity of the media (Ulaby and others, 1981). In the case of ice, σ depends on the acidity and temperature while the dielectric permittivity ε' depends on the media temperature and on the frequency of the EM signal.

Different methods have been used to define the absorption loss rate, which has been laboratory-evaluated, by measuring pure ice conductivity at different impurity concentrations and under different pressure and temperature conditions (e.g. Fujita and others, 2000; MacGregor and others 2007). Then, using a known temperature profile measured at a drilling site, ice absorption can be evaluated along the ice-core profile.

The absorption loss rate can also be calculated starting from experimental data, using ice-core measurements from drilling projects in both Antarctica and Greenland. In these cases, the availability of a known temperature profile makes it possible to scale the measured calibrated DEP along the ice core. Figure 1 shows an example with the temperature and the corrected DEP profiles from values measured at Dome C, as part of EPICA (EPICA Community Members, 2004; Wolff and others 2004). At the Dome C site the conductivity value was measured at a temperature of $-20 \pm 2^{\circ}$ C, scaled to a standard temperature of 258 K (-15°C; Stauffer and others, 2004) using the Arrhenius model (Corr and others, 1993; Paden and others 2005; MacGregor and others 2007). In the same way the ice-core conductivity profile can be corrected for the temperature of the ice along the profile:

$$\sigma(r_{\rm i}) = \sigma_{258}(r_{\rm i}) \exp\left[\frac{E}{R} \left(\frac{1}{T_{258}} - \frac{1}{T(r_{\rm i})}\right)\right]$$
(2)

where $R = 8.314472 \,\text{J K}^{-1} \,\text{mol}^{-1}$ is the gas constant and $E = 0.22 \,\text{eV}$ is the activation energy (Kulessa, 2007). The conductivity profile (σ_{258}) is known for a temperature of 258 K, r_i is the ice thickness, and $T(r_i)$ is the ice-core temperature profile. The smoothed value of ice conductivity at Dome C, calculated along an ice core 3165 m long, ranges from 3 to 13 μ s m⁻¹ (ignoring the firn layer), making it possible to consider the ice a relatively homogeneous medium.

In the assessment of the ice absorption rate using Eqn (1), dielectric permittivity was calculated using the relation $\varepsilon' = 3.1884 + (9.1 \times 10^{-4} T)$ (temperature T in °C) (Mätzler and Wegmüller, 1987). The influence of temperature on dielectric permittivity and consequently on the EM ice absorption was evaluated in the temperature range as recorded at Dome C and, in any case, was $<0.2 \text{ dB km}^{-1}$. Figure 2 (red line) reports the absorption rate using Eqn (1), calculated on the basis of the conductivity and temperature profile from the EPICA ice-core dataset. In the plot, the absorption rate varies abruptly in the first 400 m. In this range the first 100 m are influenced by the presence of firn, while below close-off the remaining part is influenced by the changes in density, dust and grain size as shown in EPICA Community Members (2004). Deeper, two different steps are clearly visible: one at -3.6 dB km⁻¹ ranging from 400 to 1560 m, and a second ranging from 1560 to 2500 m with an absorption rate that increases in magnitude to about -7 dB km⁻¹. Finally, an irregular linear trend is visible at depths below 2500 m. These steps are probably linked to the different ice acidity variation due to volcanic catastrophic events. The average value of the ice absorption rate calculated in the first step (0-1560 m) is $3.4 \pm 0.9 \text{ dB km}^{-1}$, between 0 and 2600 m (two steps) it is -5.0 ± 2.4 dB km⁻¹, while on the complete ice column it is -11 ± 3 dB km⁻¹. This



Fig. 2. Ice absorption rate at EPICA drilling site (red line) compared with those calculated by RES measurements over grouped subglacial lakes (Fig. 3).

Table 1. Complex permittivity and conductivity

Medium	arepsilon'	arepsilon''	σ $\mu S m^{-1}$
Air	1.0	0	0
Ice (–50 to –20°C)	3.18–3.22	(0.3-9) × 10 ⁻³	1–30
Rock	4–30	(3 × 10 ⁻⁶) to 3	0.01–10 000
Water	81.0	0.03-3	100–10000

last value is affected by rapid variations in conductivity in the bottom portion of the ice-core profile.

INTERFACE BETWEEN REFLECTING SURFACES

To distinguish the different physical properties of reflecting surfaces, reference is made to homogeneous horizontal surfaces.

Table 1 (Daniels, 1996; Fujita and others, 2000; Bianchi and others, 2004) lists different media with related symbols, real and imaginary parts of the complex dielectric permittivity $\varepsilon_r = \varepsilon' - j\varepsilon''$ (at a frequency of 60 MHz), conductivity and the range of considered values. The Fresnel reflectivity equation has a coefficient ρ at a separation surface between two media 1 and 2 (in the case of vertical incidence):

$$\rho = \frac{\sqrt{\varepsilon_{r1}} - \sqrt{\varepsilon_{r2}}}{\sqrt{\varepsilon_{r1}} + \sqrt{\varepsilon_{r2}}} \tag{3}$$

Power loss due to reflection *R* is equal to $|\rho|^2$, while power loss due to transmission is T = 1 - R (Ulaby and others, 1981).

Table 2 summarizes the power losses due to the reflection (R) or transmission (T) coefficients at the relative interfaces. The power loss calculated as in Bogorodsky and others (1985) is negative and must be added to the incident power (dBm). The values and their errors are calculated considering the variability ranges reported in Table 1.

In the case of a coherent flat reflector the radar equation, neglecting noise and scattering due to inhomogeneities and multiple reflections between layers, can be written as

$$p_{\rm r} = \frac{p_{\rm t} G_{\rm a}^2 \lambda^2}{\left(4\pi\right)^2 r^2} I_{\rm p} \tag{4}$$

where p_t and p_r are the transmitted and received power, G_a is the antenna gain, λ is the RES signal wavelength, r is the range from transmitting antenna, and l_p contains all the loss terms: geometrical spreading, ice absorption, losses due to the transmission and reflection coefficients T and R at the different interfaces (air, ice, ground, water, etc.) (Skolnik 1990; Peters and others 2005). The geometrical spreading l_G can easily be evaluated, knowing the time delay of the echoes (distances), as

$$I_{\rm G} = \left[\frac{G_{\rm a}\lambda}{8\pi(r_{\rm a}+r_{\rm i}/n)}\right]^2\tag{5}$$

where r_a and r_i indicate the range in air (airplane altitude) and in ice (thickness of the ice). The term l_G also contains the gain of the refractive effect when the wave propagates into the ice, characterized by the refractive index n = 1.79. The loss terms *T* and *R*, which define the reflecting EM properties at the various interfaces along the propagation path, are reported in Table 2.

 Table 2. Transmission and reflection variability ranges for several interfaces

Interface (reflection/transmission losses)	Power loss dB	
Ice/air transmission T_{ai}	0.36	0.37
Air/ice reflection R_{ai}	10.9	11.0
Ice/water reflection R_{iw}	3.49	3.51
Ice/rock reflection R_{ir}	6	25

From Eqn (4) the reflected power from the air/ice interface (ice surface) P_{ai} can be written expressing signal power in dBm (using capital letters) as

$$P_{\rm ai} = P_{\rm t} + R_{\rm ai} + L_{\rm Ga} \tag{6}$$

where R_{ai} is the power loss due to reflection at the air/ice interface and L_{Ga} is related to the geometrical loss in air (I_G at $r_i = 0$).

Following the same procedure, reflected power from the ice/water surface P_{iw} can be written as

$$P_{iw}(r_i) = P_t + 2T_{ai} + R_{iw} + 2L_i(r_i) + L_{Gr}(r_i)$$
(7)

where R_{iw} represents the attenuation of the signal power reflected from the ice/water interface that, in this analysis, is the reflection from a subglacial lake at ice depth r_i . The EM ice absorption L_i includes all the glacial power losses due to variation in density, homogeneity and temperature of the ice. Hereafter the transmission coefficient of the internal layers is ignored and considered approximately zero (MacGregor and others, 2007; Zirizzotti and others, 2012). All the terms P_{iw} , $2L_i$ and L_{Gr} depend on ice depth r_i .

Comparing Eqns (7) and (6), the loss term L_i can be assessed for generic signals reflected from the ice/water interface (subglacial lake in this case) at depth r_i and from the ice surface:

$$L_{i}(r_{i}) = \frac{(P_{iw}(r_{i}) - P_{ai} + R_{ai} + L_{Ga} - L_{Gr}(r_{i}) - 2T_{ai} - R_{iw})}{2}$$
(8)

It is worth noting here that the difference between the terms $P_{iw}(r_i)$ and P_{ai} for bottom and surface reflection levels is a sort of normalization of the received signals that enables comparison of radar traces from different campaigns with different transmitted signal levels. Moreover, this procedure allows us to evaluate only the difference between L_{Ga} and $L_{Gr}(r_i)$ which does not depend on antenna gains, with a simplification in the analysis of the radar data. Furthermore the carrier frequency used does not affect the EM ice absorption for frequencies below 300 MHz (Fujita and others, 2000).

RES MEASUREMENTS OVER SUBGLACIAL LAKES

During several Italian Antarctic RES campaigns (INGV, 2014), from 1995 to 2013, a large number of subglacial lakes were identified from analysis of the acquired radargrams (Cafarella and others, 2006) and added to the international subglacial lakes catalogue. The Dome C area was chosen as an ideal location because of its abundance of subglacial lakes and the presence of the EPICA ice core. For this analysis, 35 subglacial lakes were selected, distributed 360° around the ice-core site and located at different depths in the ice. Figure 3 reports their positions on a bedrock map



Fig. 3. Position of grouped subglacial lakes chosen for the analysis on a bedrock elevation map. Symbols indicate different ice absorption rate ranges (see legend).

(Antarctic Polar Stereographic Projection, datum WGS84), while the main characteristics (mission number, latitude and longitude coordinates and ice thickness) are reported in Table 3. Lakes have been grouped in four different zones in the Concordia area to analyze different ice properties in different zones. The analyzed radar measurements were collected during different Antarctic campaigns using several different RES systems, with different transmitted peak powers (2–4 kW), and different pulse lengths (100 ns to 1 μ s) at the same carrier frequency of 60 MHz (Zirizzotti and others, 2008).

In Table 3 the lakes are numbered according to mission number, latitude and longitude coordinates and ice thickness. The average ice absorptions were calculated over the lake extension using Eqn (8), with the transmission and reflection attenuation values reported in Table 2.

Absorption can be defined as

$$L_{i}(r_{i}) = A(r_{i})r_{i} \tag{9}$$

where $\bar{A}(r_i)$ is the averaged absorption rate (dB km⁻¹) calculated along the lake extensions. Using Eqns (8) and (9), the term *A* can be evaluated from lake RES profiles and it can be compared to the absorption rate *A* resulting from the ice-core measurements using Eqn (1). Figure 2 reports the calculated values of the average ice absorption rate $\bar{A}(r_i)$ obtained from Eqn (9) using the L_i and r_i values (Table 3) plotted together with those calculated using the EPICA measurements (colored points and red line respectively). The absorption rate has been evaluated as the ratio between ice absorption and depths. The error in the absorption rate has been evaluated using the ice absorption formula introducing the ice absorption errors and measured depth

Table 3. Subglacial lake measurements

Lake	Mission	Lat.	Long.	Depth $\Delta r_{\rm i}$ = ±42 m	Absorp. rate
				m	dB
it1	M6V1	-75.46	121.63	3569	-7.2 ± 0.7
it27	M8V1	-74.026	125.045	4078	-7.1 ± 0.7
it2	M6V1	-75.509	121.379	3585.	-7.6 ± 0.9
itl23	M25V2	-74.0633	120.0418	4096	-7.8 ± 0.9
it3	M6V2	-75.624	121.607	3504	-7.5 ± 1.0
itl6b	M25V3	-74.6486	118.6878	3980	-6.6 ± 0.9
it4	M6V2	-75.422	122.315	2990	-8.1 ± 1.3
itl6a	M25V3	-74.4149	119.5614	4048	-6.5 ± 0.9
it14	M5V3	-74.785	122.284	3422	-7.6 ± 0.8
itl21	M25V1	-75.0586	119.8538	3734	-8.6 ± 0.6
it6	M6V2	-74.412	119.497	3424	-7.4 ± 0.8
itl20	M25V1	-75.0251	121.5728	3520	-9.4 ± 1.0
it15	M5V2	-75.345	125.022	3183	-7.8 ± 1.0
itl22	M25V2	-74.8528	121.4559	3506	-7.6 ± 0.9
it17	M5V2	-75.954	126.028	2958	-7.5 ± 0.7
itl11	M25V3	-74.503	117.4569	4392	-7.9 ± 0.6
it18	M5V2	-75.811	126.526	3412	-7.0 ± 0.7
itl19	M9V1	-75.0245	122.1661	3230	-6.5 ± 0.7
it19	M5V1	-74.913	121.732	3354	-7.0 ± 0.9
it10	M5V1	-74.359	127.712	4056	-5.7 ± 0.9
it23	M5V3	-75.024	125.732	3425	-6.9 ± 0.9
it29	M8V1	-73.957	127.73	4098	-8.4 ± 0.5
it24	M5V3	-75.03	125.748	3427	-7.1 ± 1.0
it30	M8V1	-74.201	127.677	4082	-7.3 ± 0.6
it7	M6V4	-75.608	117.686	4502	-7.4 ± 0.5
it31	M8V1	-74.336	127.798	4095	-7.6 ± 0.6
it21	M5V3	-74.673	116.421	3387	-7.5 ± 0.9
it28	M8V1	-73.943	125.459	3956	-6.7 ± 0.5
it5	M6V3	-77.626	115.191	3494	-7.9 ± 0.8
it20	M5V3	-74.598	119.266	4017	-6.5 ± 0.8
it9	M5V1	-74.059	124.9	4003	-7.4 ± 0.9
it12	M5V1	-73.702	119.715	4039	-7.1 ± 0.5
it11	M5V1	-74.169	124.913	4111	-7.1 ± 0.7
it13	M5V1	-74.005	127.767	4078	-7.6 ± 0.9

errors (depending on transmitted pulse length used). The absorption error has been evaluated as the sum of errors of Eqn (8) for each lake. The errors $\Delta R_{ai} = 0.5 \text{ dB}$, $\Delta T_{ai} = 0.5 \text{ dB}$ and $\Delta R_{iw} = 0.4 \text{ dB}$ have been overestimated using 10% of the values, while the term $\Delta (LG_a - LG_r(r_i))$ is calculated with the propagation error formula in dB. The reflected powers P_{iw} , P_{ai} and their relative errors have been evaluated as mean power and standard deviation of the signal amplitude collected over the lake extensions.

The analyzed data profiles are located at different depths ranging from 2958 m (at it17; Fig. 3) to 4502 m (at it7; Fig. 3). Consequently, since the depth of the selected subglacial lakes ranges from 2960 to 4500 m, direct comparison between EPICA and RES ice absorption rate values is not possible.

The RES-based ice absorption rate values calculated from these different depths (over an area of ~16 000 km² in Fig. 3) show an average value $A_m = -7.2 \pm 1.4 \text{ dB km}^{-1}$. This value agrees (within the errors) with the ice absorption rate obtained from EPICA measurements averaged over the range 0–2600 m, and is close to the value calculated in the interval 1560–2500 m (about –7.0 dB km⁻¹, visible in Fig. 2). This value also agrees with the average absorption rate calculated from bedrock reflectivity over a smaller area (150 km × 50 km) around the EPICA drilling site as reported

in Zirizzotti and others (2010, 2012). However, here the radar measurements of the ice absorption rate are relatively constant and they are independent of depth and of different zones in the area.

Attenuation of the radar signal across the Antarctic ice sheet using a thermomechanical model has been evaluated by Matsuoka and others (2012). The average value of $\sim 10 \pm 2 \text{ dB km}^{-1}$ valid for the Dome C area is confirmed here. Jacobel and others (2010) also made careful studies of radar attenuation in East Antarctica. Although they did not cover Dome C, they found an absorption rate of $8.6 \pm 0.1 \text{ dB km}^{-1}$.

For the first time, the results described in this paper take advantage of radar measurements over lakes where reflectivity (-3.5 dB) could be considered and used as a constraint in the analyzed area. Consequently the averaged value of A_m (-7.2 dB km⁻¹) could be used as a reference value for the ice absorption rate in the area over subglacial lakes, also considering that, in general, geothermal flux and accumulation rate can affect the temperature profile and, consequently, the absorption rate over a large area (Matsuoka, 2011).

CONCLUSIONS

Over the past few years the discovery of numerous subglacial lakes has attracted scientific interest in the possible existence of water circulation between lakes and beneath the Antarctic ice sheet. For this purpose, analysis of the power of RES echoes has played a fundamental role in the characterization of basal physical conditions. The identification of subglacial lakes and/or dry-wet bedrock conditions is also extremely useful for formulating hypotheses and models of geothermal flux and ice column flow on the Antarctic plateau. While the recognition of subglacial lake surfaces is relatively easy in radargrams, understanding the ice/bedrock interface properties is usually more complicated. Signal amplitude in response to bedrock morphologies could depend on several different factors (e.g. a focusing effect, surface roughness, or changes in the EM properties of the ice column).

We have examined the latter factor and, in particular, the EM ice absorption rate obtained from RES profiles collected over subglacial lakes near Dome C, comparing the values with those obtained from EPICA ice-core drilling. The idea was to measure ice absorption starting from the radar equation with measurements taken over subglacial lakes, where the EM reflectivity value is known. The study included 35 catalogued subglacial lakes located at different depths (2960-4500 m) and arrayed $\sim 360^{\circ}$ around the ice-core site, in an aerial extension of $\sim 16\,000\,\text{km}^2$. It was found that the calculated values fluctuated around an average value of $-7.2 \pm 1.4 \text{ dB km}^{-1}$, independent of lake depth or location. This ice absorption rate value agrees with that obtained from the EPICA ice core valid in deeper ranges, and with the rate calculated over a smaller area around the drilling site $(-7.5 \pm 0.7 \text{ dB km}^{-1})$. Moreover the lakes have been grouped in four different zones and no correlation has been found between ice absorption rate value and location. Consequently, this value can be used to estimate bedrock reflectivity when it is fundamental to identify the physical status of the bedrock. It might also help to improve confidence in wetdry bedrock analysis relatively far from ice-core points, where changes in ice column absorption could mislead the interpretation of the received signal amplitude.

We conclude that ice absorption rate calculation over a district including lakes and using RES data could help to integrate the EM properties of the ice with the instrument responses, widening the significance of point data (i.e. ice cores) or providing a starting value where point data are not available.

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